

A Continuous Adiabatic Demagnetization Refrigerator for Far-IR/Sub-mm Astronomy

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Abstract. We report on recent progress in the development of a continuous adiabatic demagnetization refrigerator (CADR). Continuous operation avoids the constraints of long hold times and short recycle times that lead to the generally large mass of single-shot ADRs, allowing us to achieve an order of magnitude larger cooling power per unit mass. Our current design goal is 10 μW of cooling at 50 mK using a 6-10 K heat sink. The estimated mass is less than 10 kg, including magnetic shielding of each stage. The relatively high heat rejection capability allows it to operate with a mechanical cryocooler as part of a cryogen-free, low temperature cooling system. This has the advantages of long mission life and reduced complexity and cost. We have assembled a three-stage CADR and have demonstrated continuous cooling using a superfluid helium bath as the heat sink. The temperature stability is 8 μK rms or better over the entire cycle, and the cooling power is 2.5 μW at 60 mK rising to 10 μW at 100 mK.

1.0 INTRODUCTION

To meet the growing need for more capable low temperature refrigerators for space astronomy missions, we are developing an magnetic refrigerator that operates continuously at low temperature [1,2]. It is a multi-stage system that uses one stage to directly cool a load, and others to periodically cascade heat up to a heat sink. Since the heat transfer process does not disrupt cooling, it can be performed on a relatively short time scale (~ 1 hour). This means each stage requires proportionally less refrigerant mass than a single-shot ADR [3] would need. We project that a CADR providing 10 μW of cooling at 50 mK using a 6-10 K heat sink will have a cold mass less than 10 kg.

2.0 DESIGN

The design of an ADR depends most critically on the operating temperature, the cooling power and the heat sink temperature. For future space astronomy missions using large-format, low-temperature detectors, cooling powers of up to 10 μW and temperatures as low as 50 mK are expected to be needed. Heat sink temperatures will range from about 1 K to as high as 6-10 K. This range reflects the possible pre-cooler options, from superfluid helium dewars to mechanical cryocoolers. The latter are now being baselined for a variety of upcoming missions, including Constellation-X, so it is important to begin developing low temperature coolers that can accommodate their use. The impact of such high heat rejection temperatures is actually quite

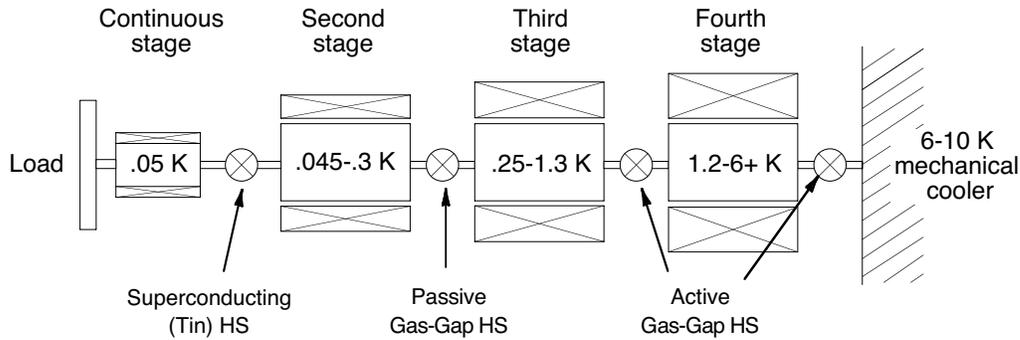


FIGURE 1. Schematic of a four-stage CADR capable of operating between 50 mK and 6-10 K.

significant since it is virtually impossible for single-stage ADRs to operate over such a wide temperature range. The multi-stage architecture of our CADR, allows us to meet this requirement with relative ease. A linear chain of ADR stages, each typically spanning a factor of 5 in temperature, can in principle operate over an unlimited temperature range.

The preliminary design for a CADR capable of operating between 50 mK and 6-10 K is shown in figure 1. Its four stages each consist of a cylindrical “salt pill” (containing the refrigerant), a magnet, magnetic shielding and a heat switch. The temperature range of each stage is determined by the properties of the heat switches. A superconducting tin switch is used between the continuous and second stages because it is one of the few types that can conduct well at temperatures below 100 mK. However its off conductance rises very rapidly with temperature, requiring the second stage to be kept below about 0.3 K at all times. Consequently the switch linking the second and third stages must be conductive at temperatures below 0.3 K. This proved challenging, but ultimately possible for a passive ³He gas-gap switch [4]. The third and fourth stages reject heat through conventional getter-activated ³He gas-gap switches.

To date, we have constructed a three-stage CADR and tested it with a superfluid helium heat sink. The as-built refrigerant masses and magnetic field strengths shown in Figure 2. Stages 1 and 2 use chrome potassium alum (CPA) refrigerant because its entropy capacity is higher than ferric ammonium alum (FAA) at temperatures below 50 mK. Its low ordering temperature will

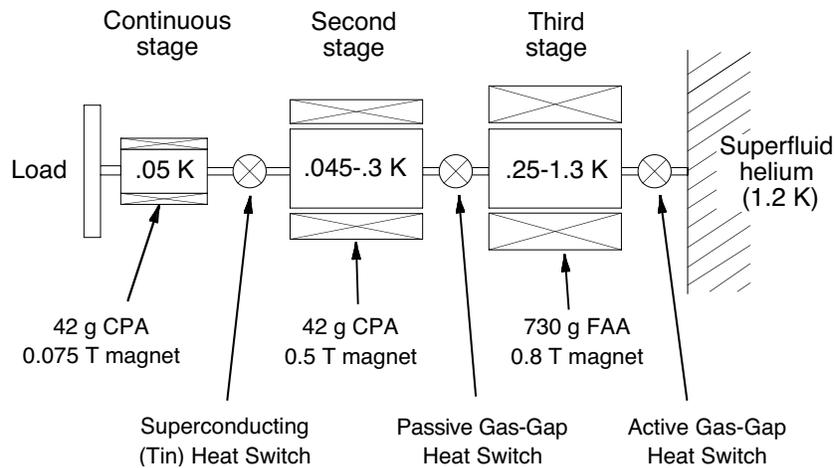


FIGURE 2. Schematic of a three-stage CADR with as-built component parameters.

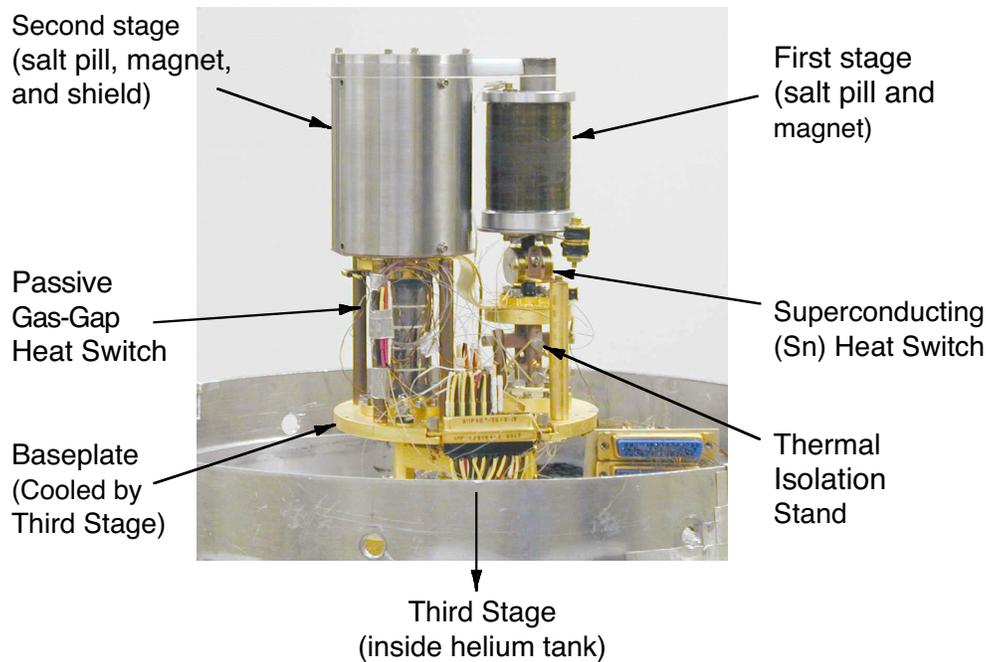


FIGURE 3. The first (right) and second (left) stages of a three-stage CADR in test configuration.

also allow the ADR to reach temperatures well below 50 mK in the event that such capability is of practical use. The third stage, using ferric ammonium alum (FAA), is an engineering unit ADR produced for the X-Ray Spectrometer mission [3], and is much larger than necessary. In the next version of the CADR, it will be replaced by an 80 g CPA salt pill, identical to the second stage salt pill, and a 1.5 T magnet. Figure 3 is a picture of the CADR in the test dewar. The third stage and its magnet are located inside the helium tank of the dewar and are therefore out of sight beyond the bottom of the picture.

3.0 OPERATION

The CADR has two operational modes. The first involves cooling down from the heat sink temperature and establishing temperature control. The second is the periodic cycling of the upper stages to maintain constant temperature.

To begin, all stages are magnetized to full field with the heat switches turned on. Starting with the third, each stage is sequentially demagnetized (after turning the appropriate heat switch off) to the low end of its operating range. The rate is not critical but should be slow enough to efficiently cool the lower stages. In the final state, the continuous stage is near full capacity and is actively cooling the load. A control routine then takes over to automatically recycle each stage as needed.

Recycling consists of demagnetizing the adjacent upper stage to a lower temperature and closing the heat switch. The temperature controller automatically magnetizes the lower stage as the upper stage absorbs its heat. When the magnetic field reaches an upper threshold, the heat switch is opened, and the upper is magnetized to the high end of its range to reject the heat to the next stage. The process is repeated until the uppermost stage rejects heat to the heat sink.

4.0 CADR PERFORMANCE

The key performance areas for a low temperature cooler are operating temperature, temperature stability, cooling power and efficiency.

4.1 Operating Temperature

To date, the CADR has operated continuously at temperatures down to 35 mK and up to 200 mK. Higher temperature operation is possible, but because of minor constraints imposed by the passive gas-gap heat switch, some software changes would be necessary in order to preserve high efficiency. These will be implemented as the need arises.

4.2 Temperature Stability

Temperature control is more of a concern for the CADR because of the need to periodically reverse heat flows into and out of the first stage. The control software minimizes the disturbances by such techniques as only turning the superconducting heat switch on and off when the temperature difference between the first and second stage is close to zero, and limiting the rate at which the heat flows can change. Another important consideration is for the temperature controllers to have fairly high bandwidth (~ 10 Hz). With both analog and digital controllers the CADR can achieve control that is limited only by the noise of the temperature readout. Figure 4 shows the temperature and magnetic field of the continuous stage during one cycle conducted at 100 mK. The magnetic field has the characteristic sawtooth pattern as heat is alternately absorbed and rejected, however there is no apparent correlation between temperature fluctuations and any recycling events. The noise is $8 \mu\text{K}$ rms or better throughout the cycle.

4.3 Cooling Power

The CADR's cooling power shown in Table 1. The cooling power is the maximum *sustainable* heat load that can be applied to the continuous stage. Although the CADR can tolerate larger momentary loads, when the heat load remains in excess of these values, the

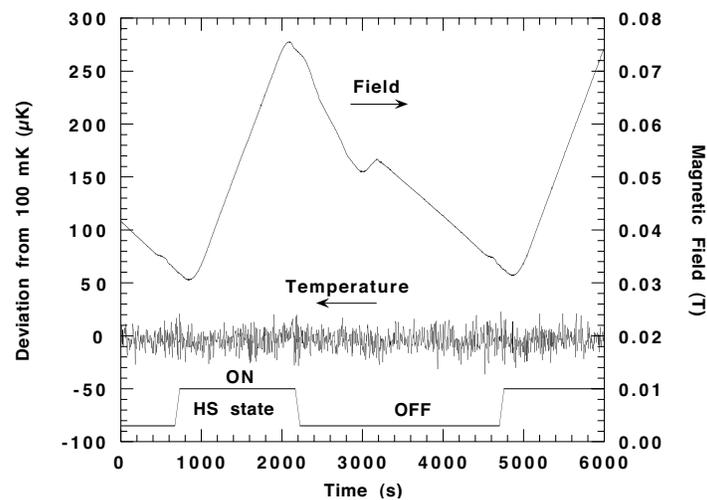


FIGURE 4. Temperature and magnetic field of the continuous stage during a complete cycle.

TABLE 1. Demonstrated Cooling Power.

Temperature (K)	Maximum Sustained Heat Load (μW)
0.10	15
0.09	13
0.08	11
0.06	7
0.05	5
0.035	1.5

continuous stage eventually runs out of cooling capacity and loses temperature control. The heat load is approximately linear in temperature above 50 mK. The non-linearity below 50 mK is due to several factors, the most important of which appear to be the rapidly increasing thermal boundary resistance between the salt and the thermal bus (which significantly reduces heat transfer efficiency), and reduced entropy capacity as the ordering temperature is approached.

4.4 Thermodynamic Efficiency

We have made careful measurements of the CADR's efficiency at both 50 and 100 mK with applied heat loads as given in Table 1. The measurement includes all parasitic effects (such as eddy current heating, magnet and magnetic shield hysteresis, heat switch and suspension system parasitics, and thermal gradients within the salt pills) except for the following: we have neglected heat that is dissipated in the third stage magnet as well as the heat applied to turn on the third stage heat switch, and we have neglected dissipation in the room temperature electronics. The reason is that these components are not yet representative of the final design, and the dissipation is consequently much higher than we eventually expect. With this in mind, we regard the measurements of 50% efficiency at 100 mK and 12% at 50 mK as being the right order of magnitude for a complete system. Granted the efficiency will decrease when the neglected terms are added, but there is also some room for improvement, for example by thermally anchoring all magnets and shields to the heat sink rather than to the third stage, as is presently the case for the second stage magnet.

5.0 SUMMARY

We have constructed a three-stage CADR that operates continuously at temperatures down to 60 mK with high cooling power. The system achieves 8 μK rms temperature stability throughout its cycling operations, and cooling powers of 2.5 μW at 60 mK rising to 10 μW at 100 mK. In the near term we will construct a fourth stage that will allow the system to operate with a 4.2 K helium bath or eventually with a mechanical cooler running at 6-10 K. We are also working on designs for suspension systems and magnetic shielding so that the system can be packaged more compactly. Our present layout for a four-stage cooler operating with a 4.2 K heat sink will fit within a 2-liter volume and weigh less than 7 kg.

6.0 ACKNOWLEDGMENTS

This work was supported by NASA's Cross-Enterprise Technology Development Program and GSFC's Commercial Technology Development Program.

7.0 REFERENCES

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